

SHORT COMMUNICATIONS

Contributions intended for publication under this heading should be expressly so marked; they should not exceed about 1000 words; they should be forwarded in the usual way to the appropriate Co-editor; they will be published as speedily as possible.

Acta Cryst. (1982). **B38**, 2092–2093

Structure of the Ni₁₁Zr₉ phase and its thermal expansion coefficient. By S. K. SHADANGI and S. C. PANDA, Department of Physics, Government College of Engineering and Technology, Raipur (MP), India and S. BHAN, Department of Metallurgical Engineering, Banaras Hindu University, Varanasi (UP), India

(Received 20 August 1980; accepted 1 February 1982)

Abstract

The Debye–Scherrer pattern of the alloy Ni₅₅Zr₄₅ clearly shows the lines of the phase Ni₁₁Zr₉, which appears to be isostructural with the phase Pt₁₁Zr₉. The unit cell of this intermetallic phase, which contains 40 atoms, is body-centered tetragonal with $a = 10.2996$ (58) and $c = 6.9359$ (42) Å. The thermal-expansion coefficient has been investigated in the temperature range 1003–1493 K.

The alloy Ni₅₅Zr₄₅ was prepared from reactor-grade Zr and Ni of 99.99% purity (Johnson Matthey & Co. Ltd, London) in a non-consumable-electrode argon arc furnace. The alloy was inverted and remelted several times to promote homogeneity. Powders obtained by filing the ingot were sieved through a 325 mesh screen and were sealed under vacuum in silica tubes for heat treatment at different temperatures.

All the X-ray patterns of this alloy could be indexed as a b.c.t. structure (Table 1). Hence it is inferred that the phase Ni₁₁Zr₉ does not undergo any phase transformation.

Table 1. X-ray diffraction data of Ni₅₅Zr₄₅ alloy, annealed at 1493 K for 30 min and quenched in water (exposure time 10 h, Cu K α radiation)

$2\theta_{\text{exp.}}$ ($^{\circ}$)	I/I_0^*	$d_{\text{exp.}}$ (Å)	hkl	$\Delta 2\theta^\dagger$ ($^{\circ}$)	$2\theta_{\text{exp.}}$ ($^{\circ}$)	I/I_0^*	$d_{\text{exp.}}$ (Å)	hkl	$\Delta 2\theta^\dagger$ ($^{\circ}$)
23.71	10	3.7517	2 1 1	+0.536	64.90	20	1.4367	4 0 4	+0.079
24.88	20	3.5784	2 2 0	+0.436	66.22	40	1.4112	3 3 4	-0.010
28.35	10	3.1477	1 1 2	-0.154	69.48	10	1.3528	7 3 0	-0.025
28.94	100	3.0850	3 0 1	-0.078	71.94	40	1.3125	5 1 4	+0.203
31.02	100	2.8828	2 0 2	-0.069	75.59	20	1.2579	{ 8 1 1	-0.111
34.94	50	2.5679	4 0 0	+0.098				{ 7 3 2	+0.143
36.00	40	2.4943	2 2 2	+0.252	79.56	20	1.2048	7 2 3	+0.154
36.98	80	2.4310	3 3 0	-0.051				{ 8 4 0	+0.001
39.27	10	2.2939	4 2 0	+0.164	84.05	40	1.1515	{ 5 0 5, 4 3 5	-0.023
40.20	20	2.2429	1 0 3	+0.264	86.52	20	1.1249	2 0 6	+0.291
43.78	60	2.0675	{ 2 1 3	-0.029	88.87	40	1.1011	9 2 1, 7 6 1	+0.175
			{ 4 0 2	-0.004	90.32	10	1.0872	3 1 6	+0.237
44.70	20	2.0272	5 1 0	-0.171	94.27	20	1.0518	5 4 5	-0.140
45.94	100	1.9753	5 0 1, 4 3 1	-0.015	97.33	40	1.0267	9 0 3	-0.134
47.32	20	1.9209	3 0 3	-0.084	99.42	20	1.0106	7 0 5	-0.168
49.48	60	1.8421	5 2 1	+0.046	101.57	20	0.99495	6 6 4	-0.059
49.99	60	1.8243	4 4 0	-0.106	105.36	20	0.96938	2 1 7	-0.107
50.79	60	1.7975	3 2 3	-0.012	113.51	10	0.92172	4 1 7	-0.130
51.78	10	1.7655	5 3 0	+0.028	121.59	40	0.85315	9 0 5	-0.089
54.14	40	1.6938	1 1 4	-0.242				{ 2 0 8	-0.020
56.00	60	1.6419	2 0 4	+0.052	128.74	10	0.85503	{ 6 1 7	+0.044
57.04	60	1.6144	4 4 2	-0.091	130.65	40	0.84835	8 2 6	+0.014
58.38	20	1.5805	5 3 2	-0.267				{ 6 6 6	-0.158
58.97	20	1.5662	{ 2 2 4	-0.025	133.96	20	0.83760	{ 3 1 8	+0.072
			{ 5 4 1	+0.032					
60.55	40	1.5290	3 1 4	+0.070	139.02	10	0.82296	7 0 7	-0.409
61.83	20	1.5004	6 3 1	-0.059	141.68	10	0.81611	3 3 8	+0.153
63.31	40	1.4688	5 2 3	+0.233	143.89	40	0.81082	9 1 6	-0.026

* Visual.

† $2\theta_{\text{exp.}} - 2\theta_{\text{calc.}}$

Table 2. Lattice parameters and thermal-expansion data of the compound Ni₁₁Zr₉ at different temperatures

Heat treatment and water quenching		a (Å)		c (Å)			
Temperature (K)	Time (min)	Observed	Calculated from linear equation	Observed	Calculated from linear equation	$\alpha_a \times 10^6$ (K ⁻¹)	$\alpha_c \times 10^6$ (K ⁻¹)
1003	70	10.1626 (58)	10.1631	6.8357 (42)	6.8346	27.50 (1)	29.10 (4)
1093	60	10.1892 (58)	10.1883	6.8538 (42)	6.8525	27.43 (1)	29.02 (4)
1223	50	10.2250 (58)	10.2246	6.8758 (42)	6.8783	27.33 (1)	28.93 (4)
1293	40	10.2558 (58)	10.2442	6.8950 (42)	6.8923	27.25 (1)	28.85 (4)
1423	60	10.2703 (58)	10.2805	6.9125 (42)	6.9181	27.21 (1)	28.77 (4)
1493	30	10.2996 (58)	10.3001	6.9359 (42)	6.9320	27.14 (1)	28.68 (4)

Kirkpatrick & Larsen (1961) have shown the existence of this phase with a b.c.t. structure but the reported parameters appear to be tentative. The correctness of the crystal structure of this phase has to be decided by comparison with the phase Pt₁₁Zr₉ (which has 40 atoms per unit cell and is b.c.t. with $a = 10.257$ and $c = 6.888$ Å) reported by Panda & Bhan (1974). Comparison shows that Ni₁₁Zr₉ is isomorphous with the Pt₁₁Zr₉ phase. This is expected as Ni and Pt are both members of the T^{10} group with ground-state electron configurations of their free atoms of $3d^8 3s^2$ and $5d^8 6s^2$ respectively and both have similar alloying behavior (Panda & Bhan, 1973).

Thermal-expansion coefficient

The X-ray photographs of the alloy Ni₅₅Zr₄₅ at each temperature were indexed and cell dimensions were determined using a least-squares treatment (Cohen, 1935, 1936). The standard errors in the lattice parameters so obtained were calculated by the method suggested by Jette & Foote (1935).

The lattice parameters vary linearly with temperature and the dependence may be expressed analytically as $a_T = 9.8828 (14) + 2.795 (13) \times 10^{-4} T$; and $c_T = 6.6351 (34) + 1.989 (31) \times 10^{-4} T$; where a_T and c_T are the lattice parameters at T K.

The linear coefficients of thermal expansion for both parameters are calculated by $\alpha_a = (1/a)(da_T/dT)$ and $\alpha_c = (1/c)(dc_T/dT)$ and are listed in Table 2.

The *American Institute of Physics Handbook* (1972) only gives the values of α for pure Ni and Zr at 293 K, but the thermal-expansion coefficient of an alloy cannot be predicted from those of its constituents (Lonsdale, 1968).

The authors are grateful to the Metallurgy Division of Bhabha Atomic Research Centre, Trombay, for melting the alloy. One of the authors (SKS) wishes to express his sincere thanks to the UGC, New Delhi, for awarding him a Teacher Research Fellowship, and also to the Ministry of Education, Government of MP, for sanctioning study leave.

References

- American Institute of Physics Handbook* (1972). Edited by E. G. DWIGHT, pp. 119–142. New York: McGraw-Hill.
- COHEN, M. U. (1935). *Rev. Sci. Instrum.* **6**, 68.
- COHEN, M. U. (1936). *Rev. Sci. Instrum.* **7**, 155.
- JETTE, E. R. & FOOTE, F. (1935). *J. Chem. Phys.* **3**, 605.
- KIRKPATRICK, M. E. & LARSEN, W. L. (1961). *Trans. Am. Soc. Met.* **54**, 580–590.
- LONSDALE, K. (1968). *International Tables for X-ray Crystallography*, Vol. III, pp. 125–129. Birmingham: Kynoch Press.
- PANDA, S. C. & BHAN, S. (1973). *Z. Metallkd.* **64**, 793–799.
- PANDA, S. C. & BHAN, S. (1974). *J. Less-Common Met.* **34**, 344–347.

Acta Cryst. (1982). **B38**, 2093–2095

On the 'riding-model' correction for bond lengths. By R. SRINIVASAN and N. R. JAGANNATHAN, *Department of Crystallography and Biophysics,* University of Madras, Guindy Campus, Madras-600025, India*

(Received 17 July 1981; accepted 6 April 1982)

Abstract

It is usual in structural reports based on X-ray or neutron diffraction methods to correct bond lengths for thermal-

motion effects. Two common procedures adopted are the riding model [Busing & Levy (1964). *Acta Cryst.* **17**, 142–146], and the rigid-body model [Schomaker & Trueblood (1968). *Acta Cryst.* **B24**, 63–76], the specific choice being dependent on the circumstances. It would appear that no critical assessment is available in the literature as to how

* Contribution No. 579.